## Type test report no. VR/R/VM/M 3E 001e

## Short circuit current test of tap selector and change-over selector

Product Approval TETP/Wag 16.07.2020

## Type test for types:

Test specification:
Test samples:

Manufacturer:
Date of test:

Place of test:
Tests performed:

## Test results:

Tap selectors of sizes "RC", "RD" and "RDE" without change-over selector, with reversing change-over selector or with coarse changeover selector, designed with 1, 2 or 3 current paths (connected in parallel) for use in combination with single phase, 2 phase or 3 phase diverter switches type VACUTAP ${ }^{\circledR}$ VR, VACUTAP ${ }^{\circledR}$ VM, OILTAP ${ }^{\circledR}$ R or OILTAP ${ }^{\circledR}$ M. IEC 60214-1:2014, sub-clause 5.2.4: "Short-circuit current test".

1: VRF III 1300 Y - 72,5/RDE - 1019 3G, S/N: 1525722.
2: R I 3003-72.5/RDE - 1019 3W, S/N: 1525721.

Maschinenfabrik Reinhausen GmbH, Regensburg, Germany.
November 2014 to December 2014.
Maschinenfabrik Reinhausen GmbH, Regensburg, Germany.
The tests were performed on one phase, on all contacts of different design carrying current continuously in service.
According to IEC 60214-1:2014 three applications were carried out with an initial peak current of 2.5 times the r.m.s. value of the rated short-circuit test current. The contacts were not moved between these applications.

|  |  | Requirement <br> IEC 60214-1 | Rated <br> values | Tested <br> values |
| :--- | :--- | :--- | :--- | :--- |
| Design variant <br> with 1 single | Initial peak current | 32.5 kA | 40.0 kA | 41.01 kA |
| current path <br> (test sample 1) | Short-circuit current (r.m.s) | 13.0 kA | 16 kA | 16.68 kA |
| Design variant <br> with 3 parallel | Initial peak current | 2 s | 3 s | 2.94 s |
| current paths <br> (test sample 2) | Short-circuit current (r.m.s) | 35.0 kA | 75.0 kA | 76.0 kA |
|  | Test duration | 2 s | 30.0 kA | 30.9 kA |

The requirements of IEC 60214-1:2014 were met, i.e.:

- At the conclusion of the test, the contacts were not damaged.
- The measurement of the initial driving torque before and after the test showed suitability for service.
- Other current-carrying parts did not show any signs of permanent mechanical distortion, which could influence the normal operation of the tap selector.

This report contains 9 pages.

i. V. Dr. Thomas Strof [valid without signature]

Maschinenfabrik Reinhausen GmbH

- PRODUCT APPROVAL .

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## 1. Test specification

The type tests were performed in accordance with IEC 60214-1:2014 "Tap-changers - Part 1: Performance requirements and test methods", sub-clause 5.2.4: "Short-circuit current test".

## 2. Data of test samples

## Test sample no.: 1

On-load tap changer: VRF III 1300 Y - 72,5/RDE - 1019 3G
Serial no. / IBASE:
1525722 / 468950866
Year of manufacture:
2014
Part of test:
Tap selector
Test sample no.:
2
On-load tap changer: R I 3003-72.5/RDE - 1019 3W
Serial no. / IBASE: 1525721 / 477030595
Year of manufacture: 2014
Part of test:
Tap selector

## 3. Scope of application

Tap selectors of sizes "RC", "RD" and "RDE" are designed on the principle of a modular system, allowing a wide range of different variations, e.g. number of contacts, number of contact planes, number of parallel current paths (per phase) and type of change-over selector. Tap selectors of sizes "RC", "RD" and "RDE" are designed for use in combination with diverter switches VACUTAP ${ }^{\circledR}$ VR, VACUTAP ${ }^{\circledR}$ VM, OILTAP ${ }^{\circledR}$ R or OILTAP ${ }^{\circledR}$ M.
Depending on the type of diverter switch the tap selector is combined with, tap selectors of sizes "RC", "RD" and "RDE" are available in following basic designs:

- Maximum rated through-current 1300 A with 1 single current path (per phase).
- Maximum rated through-current 2000 A with 2 current paths connected in parallel.
- Maximum rated through-current 3000 A with 3 current paths connected in parallel.
- Maximum rated through-current 2600 A with 2 current paths for applications with enforced current splitting.
The design of contacts that carry current continuously is identical for all tap selectors of sizes "RC", "RD" and "RDE" with reversing change-over selector, coarse change-over selector or without change-over selector.

Tap selectors of size "RDE" with 10 contacts have the maximum overall length and the minimum number of contact bars. Furthermore, types with reversing change-over selector have the longest copper connection lines.

Both the selected test samples were of size "RDE" and equipped with 10 contacts. Test sample 2 was in single phase design with three current paths connected in parallel, maximum rated through-current 3000 A and with reversing change-over selector. Concerning the occurring short-circuit stress, this variant had the most critical design. Test sample 1 was in three phase design with a single current path per phase and maximum rated through-current 1300 A (per phase). This test sample was representative for the highest maximum rated through-current per current path. The type of change-over selector was not relevant in this case.

Single phase tap selectors with 2 parallel current paths and maximum rated through-current 2000 A resp. 2600A (for applications with enforced current splitting) were not tested explicit because the rated initial peak current and rated short-time current (r.m.s) per current path are significantly lower than of test sample 1. Additionally with test sample 2 the absolute highest rated initial peak current and rated shorttime current (r.m.s) for this selector design were tested, which are significantly higher than for designs with 2 parallel current paths. Thus, tap selectors of sizes "RC", "RD" and "RDE" with 2 parallel current paths (with or without enforced current splitting) are covered by the performed tests.

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The short-circuit current capability does not depend on the insulation levels, the number of contacts and the type of diverter switch (VACUTAP ${ }^{\circledR} \mathrm{VR}$, $\mathrm{VACUTAP}^{\circledR} \mathrm{VM}$, OILTAP ${ }^{\circledR}$ R or OILTAP ${ }^{\circledR} \mathrm{M}$ ) the tap selector is combined with.

Therefore this type test report is valid for all tap selectors with following characteristics:

- Tap selector size:
- Change-over selector:
- Combined diverter switch:
- Maximum rated through-current:
- Number of phases:
- Parallel current paths (per phase):
"RC", "RD" or "RDE"
without, reversing or coarse change-over selector
VACUTAP ${ }^{\circledR}$ VR, VACUTAP ${ }^{\circledR}$ VM, OILTAP ${ }^{\circledR}$ R or OILTAP ${ }^{\circledR}$ M
1300 A, 2000 A, 2600 A and 3000 A
1, 2 or 3
1, 2 or 3


## 4. Test arrangement

Schematic test circuits:
Position and connection:
Surrounding medium:
Adjustment and measurement:

Testing transformer:
Condition of the test sample:
Servicing during the tests:
Recording and evaluation:

See figure 1 a (test sample 1 ) and figure 1 b (test sample 2 ).
See figure 1 a (test sample 1) and figure 1 b (test sample 2 ).
Transformer oil according to the requirements of IEC 60296.
Short-circuit current adjusted by air-core reactor and measured by
Rogowski transformer, see figure 1a and 1b.
The initial driving torque before and after the short-circuit current tests was measured by torque sensor and transient recorder.
$4000 \mathrm{kVA}, 20 \mathrm{kV}$, open-circuit voltage $\mathrm{U}_{0}$ : >50 V.
Temperature rise of contacts test carried out before.
No servicing during the tests.
Each test was recorded and evaluated by transient recorder.


Figure 1a: Schematic test circuit and connection of the test sample (test sample 1).


Figure 1b: Schematic test circuit and connection of the test sample (test sample 2).

## 5. Required short-circuit strength acc. to IEC 60214-1:2014

| Test sample no.: | 1 | 2 |
| :--- | :---: | :---: |
| Maximum rated through-current: | 1300 A | 3000 A |
| Number of tests: | 3 | 3 |
| Initial peak current: | 32.5 kA | 75.0 kA |
| Short-circuit current (r.m.s): | 13.0 kA | 30.0 kA |
| Test duration: | 2 s | 2 s |

## 6. Tests performed

The test was performed on two test samples. Test sample 1 was in 3 phase design with one single current path per phase and maximum rated through-current 1300 A. Test sample 2 was in single phase design with 3 current paths connected in parallel and maximum rated through-current 3000 A .
Table 1 a shows the tested short-circuit values of test sample 1 and table 1b shows the tested short-circuit values of test sample 2 . Figures $2 \ldots 7$ show recordings of the performed applications.

| Application <br> no. | Initial peak <br> current <br> $\mathrm{I}_{1 p}$ | Short-circuit <br> current <br> $\mathrm{I}_{1}($ r.m.s) | Short-circuit <br> duration <br> t | Equivalent <br> short-time current <br> (r.m.s) |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 41.06 kA | 16.69 kA | 2.93 s | $16.5 \mathrm{kA} \mathrm{-} \mathrm{3} \mathrm{s}$ |
| 2 | 41.19 kA | 16.68 kA | 2.95 s | $16.5 \mathrm{kA} \mathrm{-} 3 \mathrm{~s}$ |
| 3 | 40.92 kA | 16.67 kA | 2.93 s | $16.5 \mathrm{kA} \mathrm{-} \mathrm{3} \mathrm{s}$ |
| Mean values | 41.01 kA | 16.68 kA | 2.94 s | $16.5 \mathrm{kA} \mathrm{-3} \mathrm{~s}$ |

Table 1a: Tested short-circuit current values of test sample 1 (Design variant with one single current path).

| Application <br> no. | Initial peak <br> current <br> $\mathrm{I}_{1 \mathrm{p}}$ | Short-circuit <br> current <br> $\mathrm{I}_{1}$ (r.m.s) | Short-circuit <br> duration <br> t | Equivalent <br> short-time current <br> (r.m.s) |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 75.85 kA | 30.91 kA | 2.91 s | $30.4 \mathrm{kA} \mathrm{-} \mathrm{3} \mathrm{s}$ |
| 2 | 75.97 kA | 30.85 kA | 2.91 s | $30.4 \mathrm{kA} \mathrm{-} \mathrm{3} \mathrm{s}$ |
| 3 | 76.15 kA | 30.89 kA | 2.91 s | $30.4 \mathrm{kA} \mathrm{-} \mathrm{3} \mathrm{s}$ |
| Mean values | 76.0 kA | 30.9 kA | 2.91 s | $30.4 \mathrm{kA} \mathrm{-} \mathrm{3} \mathrm{s}$ |

Table 1b: Tested short-circuit current values of test sample 2 (Design variant with 3 parallel current paths).

Table 2 shows the measured initial driving torque of both test samples before and after the test.

| Timing of measurement | Initial driving torque <br> test sample 1 | Initial driving torque <br> test sample 2 |
| :--- | :---: | :---: |
| Before the test | 106.3 Nm | 140.3 Nm |
| After the test | 108.0 Nm | 142.6 Nm |

Table 2: Measurement of the initial driving torque.
Table 3 shows the tap selector variants covered by this test.

| Maximum rated <br> through current | Number of <br> (parallel) current <br> paths | Enforced current <br> splitting | Rated <br> initial peak current | Rated <br> short-time current <br> (r.m.s) |
| :---: | :---: | :---: | :---: | :---: |
| 1300 A | 1 | no | 40.0 kA | $16.0 \mathrm{kA}-3 \mathrm{~s}$ |
| 2000 A | 2 | no | 60.0 kA | $24.0 \mathrm{kA}-3 \mathrm{~s}$ |
| 2600 A | 2 | yes | 65.0 kA | $26.0 \mathrm{kA} \mathrm{-} \mathrm{3} \mathrm{s}$ |
| 3000 A | 3 | no | 75.0 kA | $30.0 \mathrm{kA} \mathrm{-} \mathrm{3} \mathrm{s}$ |

Table 3: Tap selector variants covered by this type test.

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Figure 2: Test sample 1 (single current path) - Recording of application no. 1.


Figure 3: Test sample 1 (single current path) - Recording of application no. 2.

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Figure 4: Test sample 1 (single current path) - Recording of application no. 3.


Figure 5: Test sample 2 (3 parallel current paths) - Recording of application no. 1.

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Figure 2: Test sample 2 (3 parallel current paths) - Recording of application no. 2.


Figure 3: Test sample 2 (3 parallel current paths) - Recording of application no. 3.

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## 7. Test results

The requirements of IEC 60214-1:2014 "Tap-changers - Part 1: Performance requirements and test methods", sub-clause 5.2.4 "Short-circuit current test" were met.

The contacts were not damaged, therefore the capability of carrying the maximum rated through-current was not reduced.

The measurement of the initial driving torque before and after the test showed suitability for service.
Other current-carrying parts did not show any signs of permanent mechanical distortion, which could influence the normal operation of the tap selector.

